

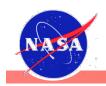




Low Density Supersonic Decelerator Technology Demonstration Mission

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Abstract



Supersonic Inflatable Aerodynamic Decelerator

• The heady days of sticking a rocket under your gizmo just to see if it works are coming back. In the summer of 1972, the Viking Project conducted four high-altitude tests in Earth's atmosphere of the supersonic parachute design to be used for landing on Mars. We've been stuck with that design ever since. In late 2013 and early 2014, a series of balloon-launched, rocket-propelled tests of the next generation of supersonic decelerators will culminate the development program of new descent technologies to be used on future Mars landers. A Mach 3.5 inflatable decelerator and a Mach 2 ringsail parachute will team to create a low-density supersonic decelerator system for high ballistic coefficient entry systems at Mars.

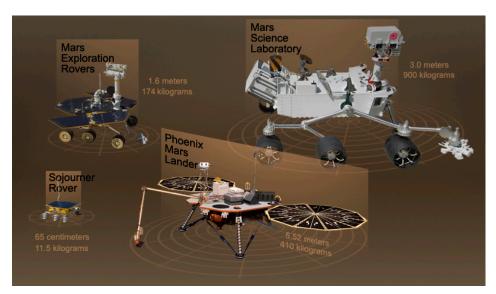


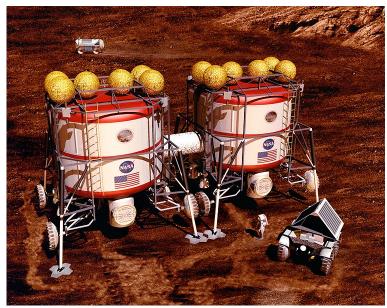


Problem



- As Mars landers grow, ballistic coefficient (β) goes up (square-cube law problem) — currently at ~1000 kg useful landed mass for MSL
- Launch vehicle fairing size not going up, lift / drag not going up



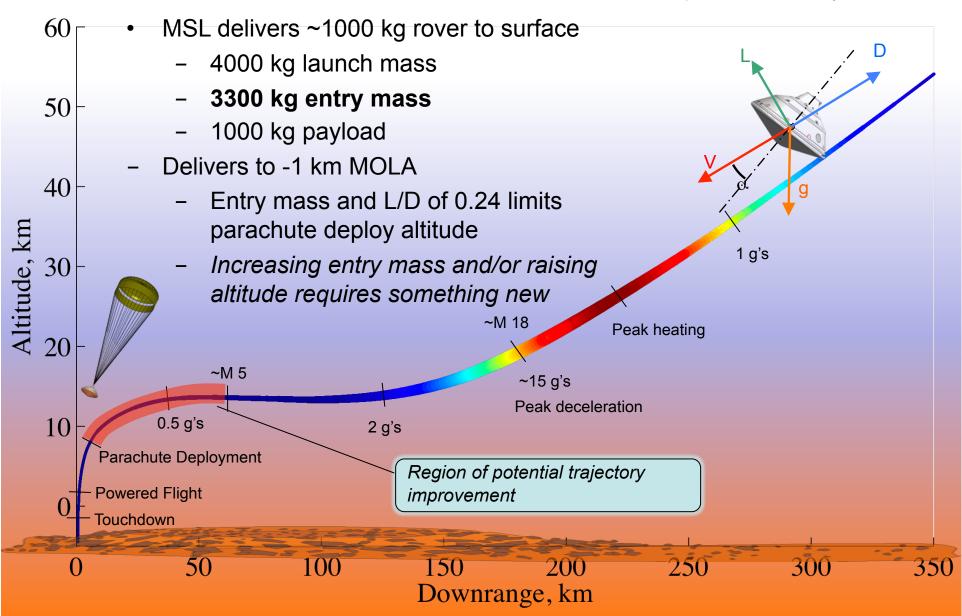


- Need to deploy a parachute at Mach ~2, but …
- As β keeps going up, eventually we hit the ground at Mach > 2
- Need to begin the scale-up to crewed Mars landers ~50,000 kg (!)
- What can we do before these things hit the ground?



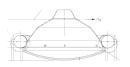
MSL Problem Area







Solution Trade Space



- Lower β or increase L/D (pull up)?
 - 1. $\beta \sim \text{mass}$ / area, so increase the area (recall mass is going up)
 - 2. Develop new entry vehicle shape and hypersonic maneuvering capability
- This effort addresses Door #1
 - Potentially some other technology development could work on Door #2
- When to increase the area?
 - 1. Increase the area before launch (new launch vehicle development)
 - 2. Increase the area before entry (high heating, but see HIAD talk next)
 - 3. Increase the area just in time, before you hit the ground, ~ Mach 3 to 5 (easiest)
- How to increase the area?
 - 1. Deployed fabric structure (low mass, low cost)
 - 2. Deployed rigid structure (higher mass, higher cost)
- What is the fabric structure?
 - 1. Parachute (poor drag at high Mach, inflation complex and problematic)
 - 2. Inflatable aerodynamic decelerator (good drag at high Mach, simple)



Supersonic Inflatable Aerodynamic Decelerators

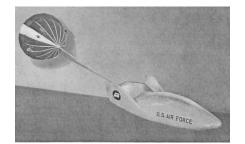


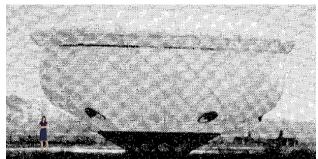
Supersonic Inflatable Aerodynamic Decelerator

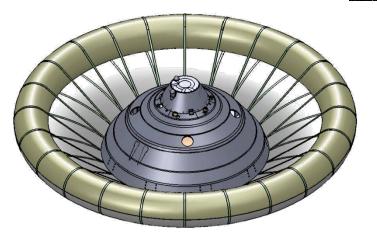
 Various kinds of Inflatable Aerodynamic Decelerators were studied and tested in the 1960's

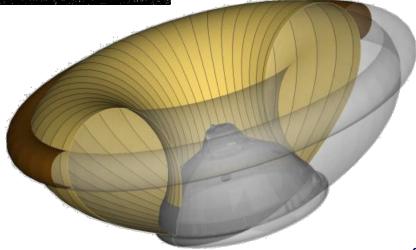
After Viking, IAD research effectively ceased

 Now that we've tapped out the Viking technology, we are revisiting IADs



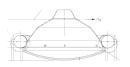




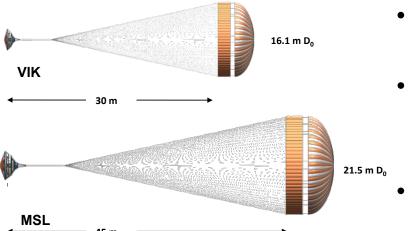




Parachute / Vehicle Diameter Heritage



Supersonic Inflatable Aerodynamic Decelerator

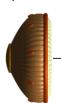


- 45 m 30.0 m D₀

Next Generation

6 m SIAD

- Preserving geometry retains system level aerodynamic heritage
- Preservation of system heritage may break piece part heritage
 - Increases qualification effort
- Larger parachutes increase landed mass and/or propellant load
 - 30 m parachute will increase mass delivery (fuel for propulsive cleanup and/or additional mass margin)
 - Parachutes growth has some limit
 - Terrestrial parachutes as large as 45 m have been tested



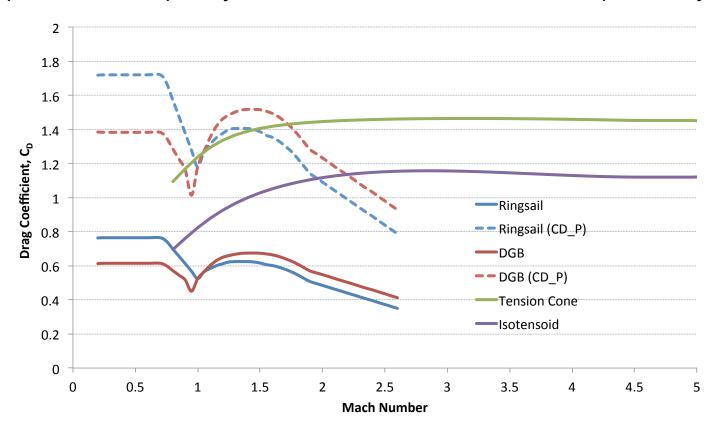
Next Generation 20 m SIAD



SIAD and Parachute Drag vs. Mach



- SIADs and parachute complement each other well
 - Just as SIAD drag is starting to fall off in Mach, parachute drag is up
- Drag fall-off makes a subsonic SIAD impractical
 - Might like to get to subsonic before parachute deploy, or eliminate parachute completely — however the SIAD becomes impractically large





Low-Density Supersonic Decelerator System



- SIAD needs to be paired with a larger parachute
 - Preserve diameter ratio heritage to avoid new wake effects region
 - Larger parachute required in order to cash in on SIAD benefits
 - Greater entry mass converted to greater terminal descent propellant mass and/ or greater payload mass
 - Altitude provides timeline for larger parachute deploy
- Viking DGB heritage has been extended to its limit by MSL
 - Viking did one supersonic test of a 19.7 m DGB
 - MSL is using a 21.5 m DGB
- A ringsail configuration provides improved performance over DGB
 - More mass-efficient drag
 - Greater stability
 - Improved inflation behavior (but to be demonstrated supersonically)
- LDSD will develop and test both a SIAD and a new supersonic ringsail parachute



SIAD and Parachute Size and Deploy Mach

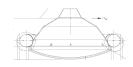
Supersoni¢

- Application trade study performed covering a wide range of SIAD and parachute sizes, entry masses, and altitudes
- Targeted improvements:
 - Entry mass 3300 kg to 4200 kg (max for Atlas V 551)
 - Landed altitude from -1 km MOLA to +2 km MOLA
 - Increased timeline for SIAD and parachute range triggers
- SIAD
 - 6 m diameter (63% increased area over 4.7 m aeroshell)
 - Mach 3.5 deploy
- Ringsail Parachute
 - 30 m D0
 - Mach 2 deploy
- Extended improvements:
 - Entry mass to 5825 kg (Delta IVH max), same altitude
 - 9 m diameter SIAD, same size parachute, same deploys





Have to Fly Them



- The qualification of soft-goods deployables requires testing of the devices at full-scale in a relevant environment
 - The motion of the soft-goods at very small scales is critical to the overall behavior of the system, making simulation impractical



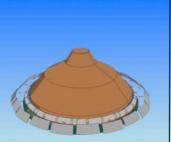


SIAD Testing



Supersonic Inflatable Aerodynamic Decelerator

Phase 1: Initial Deployment & Inflation



Parameters/Components

Cover Panel System release

SIAD packing methodology

Gas Generator performance

GG infl. @ pressure & temp.

Cover Panel System

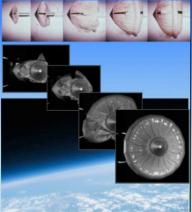
interaction with SIAD

Dynamic Pressure

GG infl. @ Q

of Interest

Phase 2: Inflation Dynamics



Parameters/Components of Interest

SIAD inflation dynamics CPS behavior Vehicle dynamics

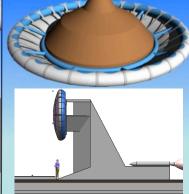
Relevant Test Environment | Relevant Test Environment | Static Pressure | Mach Number

Mach Number Static & Dynamic Pressure

Method of Qualification Method of Qualification

IAD deployment in a relevant Mach-Q flowfield, while attached to a relevant blunt body capsule.

Phase 3: Deployed Strength and Integrity



Parameters/Components of Interest

Qualification Load on IAD IAD Inflated shape

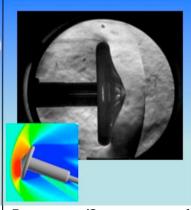
Relevant Test Environment

Dynamic Pressure

Method of Qualification

Aerodynamic loading of SIAD to test load.

Phase 4: Supersonic Performance



Parameters/Components of Interest

IAD Inflated shape Static Aero coefficients Dynamic Aero coefficients Stiffness effects

Relevant Test Environment

Mach Number
Dynamic Pressure
Non dimensional parameters

Method of Qualification

Supersonic IAD flights closely coupled with CFD analysis and subscale supersonic testing

Phase 5: Subsonic Performance



Parameters/Components of Interest

IAD Inflated Shape Parachute configuration Static Aero coefficients Dynamic Aero coefficients

Relevant Test Environment

Mach number Dynamic Pressure

Method of Qualification

Subsonic flight of IAD



Parachute Testing



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Phase 1: Parachute Mortar Deployment	Phase 2: Initial Inflation of Parachute	Phase 3: Initial Inflation Strength	Phase 4: Supersonic Performance	Phase 5: Subsonic Performance
Parameters/Components of Interest Deploy bag design Line stretch mechanics Packing methodology Bag strip mechanics Deploy bag retention	Parameters/Components of Interest Canopy inflation dynamics Parachute design Flow field	Parameters/Components of Interest Flight Limit Load on Parachute (81k#)	Parameters/Components of Interest Parachute configuration Drag coefficients Mach efficiency curve Stability coefficients Area oscillation	Parameters/Components of Interest Parachute configuration Drag coefficients Mach efficiency curve Stability coefficients
Relevant Test Environment Mortar ejection velocity	Relevant Test Environment Mach Number Flow Velocity Parachute Design Wake Structure	Relevant Test Environment Dynamic Pressure	Relevant Test Environment Mach Number Flow Velocity Parachute Design Wake Structure	Relevant Test Environment Flow Velocity Parachute Design Wake Structure
Method of Qualification Mortar ejection	Method of Qualification High Altitude supersonic parachute deployments.	Method of Qualification High Altitude/High velocity parachute deployment.	Method of Qualification High Altitude supersonic parachute flight.	Method of Qualification High Altitude subsonic parachute flight.
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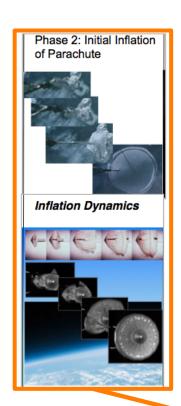


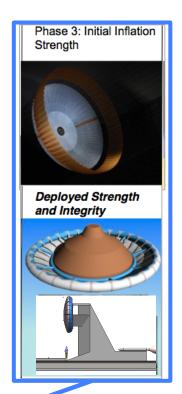
Test Types



Supersonic Inflatable Aerodynamic Decelerator











Design Verification

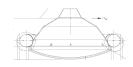
Full scale hardware testing to verify design functionality & integrity

Flight Dynamics

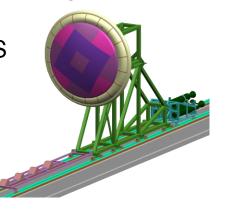
Supersonic and subsonic flight testing to verify flight dynamics and aerodynamic performance



Design Verification Tests



- Design Verification Tests (low cost, repeated by infusing project)
 - Dynamic pressure but not Mach is replicated to test the strength and operation of the devices
 - Allows over-testing of strength which is not feasible for at-Mach testing
 - Lower cost tests to assure working devices before at-Mach testing
 - Parachute dropped from high-altitude balloon
 - SIAD on rocket sled at China Lake NAWS



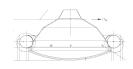


- SIAD low pressure inflation testing
 - Rocket sled at ground uses higher-pressure inflation system
 - Test low-pressure SIAD inflation and deployment at Plum Brook





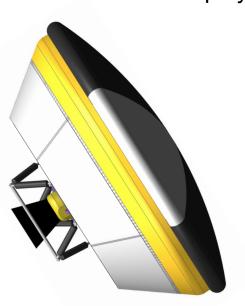
Flight Dynamics Tests

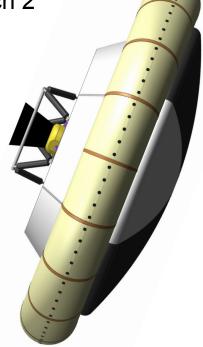


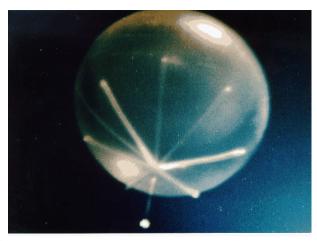
Supersonic Inflatable Aerodynamic Decelerator

- Viking-style balloon drop (high cost, not repeated by infusing project)
 - Full-scale (4.7 m aeroshell) test vehicle dropped from high-altitude balloon
 - Solid-rocket motor in test vehicle accelerate to Mach 4 (spun for stability, then despun)
 - SIAD deployed at Mach 3.5

Parachute deployed at Mach 2







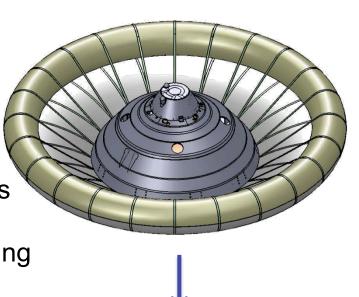


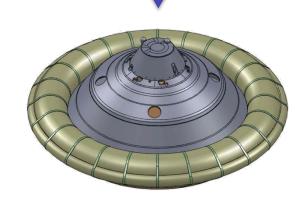


Extensibility 1: SIAD Rigidity Hypothesis



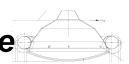
- 6 m SIAD size results in a "degenerate" tension cone — the cone part goes away
- Left with an "attached torus" configuration
- At sufficient pressure, an attached torus should behave like a rigid structure
- If it does, then new rigid SIAD configurations could be developed and dynamic behavior determined in lower cost ballistic range testing
- This would allow greater extensibility of the LDSD developments to new designs
- LDSD will test the rigidity hypothesis for the attached torus configuration



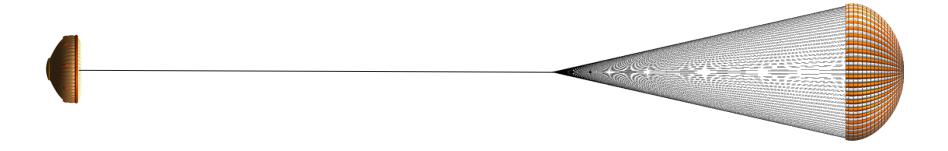


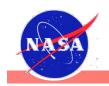


Extensibility 2: Breaking Diameter Ratio Heritage



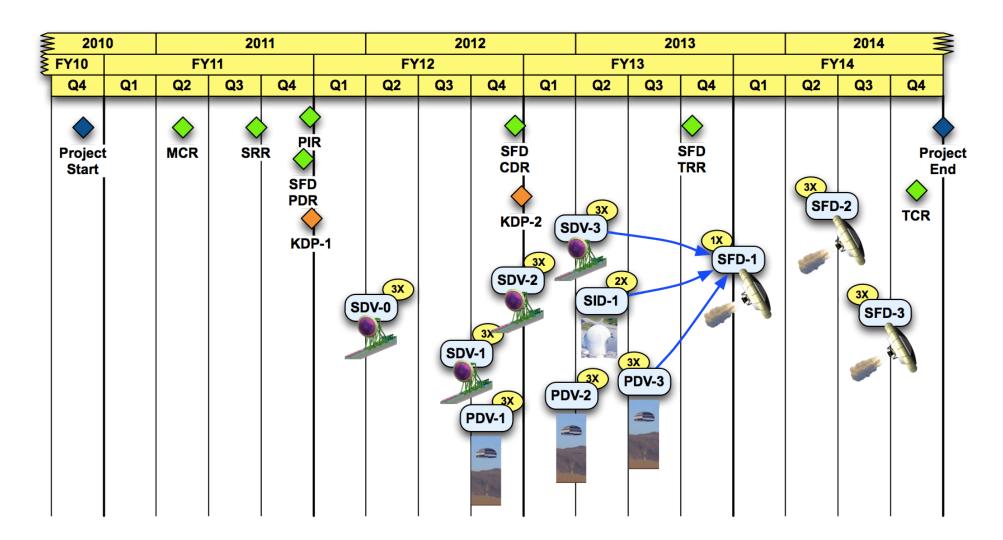
- LDSD also plans to test configurations with larger ~9m SIADs
 - But not with a larger parachute, so not preserving diameter ratio
- Prepare for very large Mars landers (Delta IVH-class)
- Explore low ratios of parachute to SIAD diameter and wake effects
- Explore non-rigid SIAD configurations
- Provide data for future CFD and FSI work on these systems
 - Some CFD and FSI work will be done as part of the LDSD project in order to inform the measurements strategy





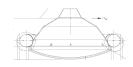
LDSD Testing Timeline







LDSD Status



- LDSD will complete its formulation phase in October
 - Will enter implementation in FY12
- SIAD development
 - Conducted three industry studies on SIAD configurations and construction
 - Awarded contract for SIAD fabrication (ILC Dover), kickoff in two weeks
- Test development
 - Rocket sled fabrication will begin next month
 - Preliminary design approaches for supersonic flight testing complete
- Have been working to \$12M funding through FY11
- Total estimate LDSD project cost: \$160M
- LDSD is a line item in the President's FY12 budget submission
 - Total run-out of \$148M through FY14 (plus current \$12M = \$160M)
- LDSD dependent on NASA OCT receiving funding in FY12
 - Not a given due to propensity of Congress to operate the country on continuing resolutions — OCT not funded in current operating budget